

resolution of the equations, but it can produce infinite gain as infrared approaches dust gray. The singularity that exists as visible and infrared approach the dust gray level is ameliorated by the average over the entire block; however, as a further refinement, the formula can be made less subject to such artifacts by moving the singularity to a pure black infrared number by substituting the formula  $x=G+(V-G)/IR$  in function block 724.

The operation of the gain and specific formulas given above are given further intuitive foundation in FIG. 11. FIG. 11a illustrates how the visible record is affected by different degrees of defects. When infrared=unity, there is no defect, and so visible=x. A small defect may attenuate infrared to 0.8, and visible will therefore also be the same 0.8 when x=white. However, the visible line 1102 will pivot on the dust gray point 1104. The extreme refractive defect will pull infrared, and the visible level when x=white, all the way down to dust gray, which will pivot on dust gray 1104 to give the horizontal line 1106. The horizontal line implies no image is seen, whether x=black or x=white, only the dust gray of the defect will be seen.

To undo the effects of a defect, the visible record will need to be amplified to overcome the masking effect of the defect. The amplification should be relative to dust gray. FIG. 11b illustrates how a gain is chosen to multiply the visible record such that visible times gain is an estimate of x. Note that when infrared=dust gray, gain goes to infinity in an attempt to see through an opaque defect. Although theoretically correct, this singularity creates gross artifacts in actual systems with deviations from perfection, and is avoided by the offset method taught above.

The concept of a correction range was already presented in connection with FIG. 4 in range blocks 450 and 452 acting with the smart subtraction block 460 as defined. This concept of a correction range will now be applied to the method of FIG. 7.

In FIG. 7, let the gain block 730 go to zero, thereby eliminating it from the operation. In its place let the upper bound gain block 770 follow the line 1022 of FIG. 10, such line defining the relationship of input x to output gain, and further let the lower bound gain block 772 follow the line 1020 of FIG. 10. The upper bound gain 770 multiplies each element of the infrared transform block 712 at multiplier 774 to give the upper bound limit transform 776, and similarly the lower bound gain 772 multiplies block 712 at multiplier 778 to give the lower bound block 780. The upper and lower bounds are subtracted from the image transform 710 by the smart subtraction function 744, in effect using whichever bound brings the result closest to zero, and outputting zero when zero is in between the result of both bounds, thereby totally nulling defects that are within the crosshatched uncertainty range 1024 of FIG. 10.

A further refinement makes the nulling range frequency sensitive to accommodate a greater uncertainty range at higher spatial frequencies, as mentioned above. To practice this frequency dependence, the upper and lower gain blocks 770 and 772 are made frequency dependent. In particular, a low frequency element 722 in the infrared transform may be multiplied by upper and lower bound numbers defined by center line 1010 of FIG. 10, whereas a higher frequency element 788 located a distance 790 from the low frequency element 722 would be multiplied by upper and lower bound lines 1022 and 1020 respectively of FIG. 10. Finally, a very high frequency term 792 would be multiplied by upper and lower bound lines 1002 and 1004 respectively. This method enables more aggressive removal of defects at the higher frequencies.

The examples discussed so far have input a single visible image for processing. It should be understood that a full color image could be processed by repeating the described process with a red visible image, a green visible image, and a blue visible image.

The preferred embodiment disclosed with reference to FIG. 7 used a block transform structure; however, the use of such a structure is not a limitation in the practice of the present invention. Other structures permit the multiplication of infrared defect detail by a gain that is determined as a function of visible image brightness in such a way that defects can be corrected from highlights to shadows. As an example, FIG. 12 presents an alternate embodiment of the invention that uses neither blocks nor a frequency transform space.

In FIG. 12, a visible image 1202 is received along with a registered infrared image 1204. The specific mathematics of this example will assume these images are in linear space, but as explained above, other gamma corrected spaces may be used. At function block 1206 a small amount of the visible image 1202 is subtracted from the infrared image 1204 to yield an infrared image 1208 free of visible traces 1210. In practice, a small amount of the cyan record, as seen in the red visible scan, will appear in the infrared scan 1204 as a smudge 1210. This can be eliminated by moving the wavelength of the infrared scan farther from the visible spectrum, but high wavelength infrared can stress the optics and sensors used in the scanner. In practice, as an expedient, the infrared scan is kept rather close to the visible spectrum under a wavelength around 850 nm, and the residual effect of the visible image is removed by subtracting about 10% of the red visible record. This step could also be applied to any of the examples previously described if needed.

In the example of FIG. 7, the details of the infrared defect scan were separated in frequency as is the nature of a DCT or DFT transform. That is, where there is no defect detail, the film is clear in infrared, and all elements of the infrared transform, except the average term, are zero, and any multiplication of the zero terms by a gain will have no effect on the zero value in that term. Conversely, where there are defects, the transform terms will be nonzero, and will be affected by a multiplication in proportion to the level of the defect. In the present example of FIG. 12, defect details are separated by grayscale. Assuming the image has been normalized such that image 1208 is unity for a section of the image with no defects, function block 1214 subtracts unity from image 1208 to result in an image 1216 that is zero at points with no defect, and as image 1208 drops below unity, image 1216 goes negative in proportion to the depth of the defect. Thus the detail of the defect record has been isolated in image 1216 in such a way that only detail; i.e., nonzero points of the image, will be affected by any multiplication of pixels in the image 1216.

While the defect details are being isolated in image 1216, the gain that will be applied to those defect details is being calculated for each pixel. The visible image is blurred by function block 1220 to form blurred visible image 1222, and the infrared image is blurred by function block 1224 to form blurred infrared image 1226. This blurring reduces artifacts in the calculation of gain caused by irregularities and noise in the image. A typical blur is to average a 9x9 pixel box around each pixel in image 1202 or 1204 to assign the corresponding pixel in blurred image 1222 or 1226.

Next, for each pixel in the blurred visible image 1222, x is estimated in conjunction with the corresponding pixel in the blurred infrared image 1226 by estimator 1228. The