

flows into the chamber 30 and the chamber 30 is allowed to pressurize and expand the Braille dot 20. In this the Braille dot 20 is formed by distorting the top surface 46 attached to the frame 24 (which may be part of the housing 22 module 18 and is not shown in FIG. 5A or 5B). The Braille dot 20, is just a dimple in the top surface 46. Referring now to FIG. 5B, voltage is applied to electrode 281a and the slide element 28 is attracted to it closing the passage to the plenum 32 and opening the passage to the vent 33 and allowing the pressure to vent out of the chamber 30. Without the pressure, the Braille dot 20 contracts, flattening out the Braille dot in the top surface 46. The voltage to the electrodes 281a, 281b is controlled by either the microcontroller 40 through lines 44 or the module microcontroller 45 through lines 44 allowing independent extension and retraction of the Braille dots 20.

Referring now to FIG. 6 there is shown a schematic representation of the Braille dots 20 electronic addressing scheme. The Braille dots 20 are actuated based upon a row and column scanning mechanism. Although, only 4 rows and 5 columns are shown on FIG. 6, the scanning mechanism can be applied to any number of rows and columns. If at any time "t" both the row and column are at open electrode voltage (signified by "0") the MEMS device is open and the Braille dot 20 is extended. If either the row or the column is at close electrode voltage (signified by "1"), the MEMS device 16 is closed and the Braille dot 20 is retracted. In this manner, at any time "t" a specific Braille dot 20 based upon its row and column location can be operated. For example, at t<sub>1</sub> row 1 has open electrode voltage and column 1 has open electrode voltage. The Braille dot 20 is extended as shown by the X on the actuation scheme.

Referring now to FIG. 7, there is shown an internal elevation of the housing 22. In this FIG. 7, the modules 18 are mounted to the inside of the housing 22 near its top. The top surface 46 attaches to the top of the housing 22. The top surface 46 is constructed of a single sheet of polymer material stretched over the top of the housing 22. The top surface 46 presents a continuous surface which provides both environmental protection to the MEMS devices 16 (not shown in FIG. 7) and other electronic hardware as well as providing a tactile surface with no discrete holes, seams, gaps or voids. In the present invention a low modulus elastomer with a thickness of approximately 0.004" is used for the top surface 46. Two commercially available elastomer films can be used; a medium modulus latex polymer mix, or a blend of Natural Rubber, Neoprene and Nitrile. The top surface 46 is sealed to the modules 18 and/or housing 22 using either a suitable epoxy or adhesive or a vacuum seal. This provides a continuous uninterrupted tactile reading surface for the user eliminating any interference with reading of Braille characters 14. This modular design allows different size Braille displays 2 to be assembled from a different number of individual modules 18.

Referring now to FIGS. 8A and 8B there are shown detail views of a Braille dot 20 with a MEMS device 16 extended and retracted, respectively. The actuators are a pair of MEMS microvalves 284a, 284b which open or close. The MEMS microvalves 284a, 284b can be actuated electrostatically, piezoelectrically or using thin film shape-memory alloys. In FIG. 8A, the MEMS microvalve 284a is open allowing pressurized air from the plenum 32 into the chamber 30, while the MEMS microvalve 284b is closed blocking the pressurized air from leaving the chamber 30. The pressurized air in the chamber 30 expands the Braille dot 20. In this the Braille dot 20 is formed by distorting the

surface covering 45 attached to the frame 24 (which may be part of the housing 22 module 18 and is not shown in FIG. 8A or 8B). The Braille dot 20, is just a dimple in the top surface 46. Referring now to FIG. 8B, the MEMS microvalve 284a is now closed blocking the flow of pressurized air from the plenum 32 and the MEMS microvalve 284b is now opened allowing the air to evacuate from the chamber 30 to the vent 33. With the pressure vented, the Braille dot 20 contracts, flattening out the dimple on the top surface 46. The voltage to the two the MEMS microvalves 284a, 284b are controlled either directly by the microcontroller 40 or by the module microcontroller 45 to extend and retract Braille dots 20 independent of other Braille dots 20.

Referring now to FIGS. 9A and 9B there is shown a detail view of a Braille dot 20 and MEMS device 16 which uses a thin film shape memory alloy ("SMA") element 282 as the actuator. A thin film SMA based microelectromechanical actuator is significantly different then traditional bulk shape memory alloy actuators in size, fabrication techniques, and operation. The mechanical properties of a thin film SMA can be precisely tailored by changing the alloy ratios during fabrication while a macro sized bulk SMA actuator may have regions where the alloy ratio changes within the bulk material of the actuator, these regions will increase power consumption, reduce fatigue resistance and limit life. Thin film SMA actuators have greater fatigue life and improved phase transition characteristics then traditional bulk SMA actuators. The thin film SMA also has faster response and lower power consumption then traditional bulk SMA actuators due to their reduced volume and large surface area which allows the actuator to change from one phase state to another faster then the larger bulk SMA actuators. The rapid response of the thin-film SMA actuators allows a user to quickly scroll through a document without having the refreshable Braille display lag behind. The lower power consumption of a thin film SMA actuator reduces the amount of heat that needs to be dissipated from the actuators during operation and can permit battery operation for use with portable electronic devices.

FIGS. 9A and 9B also show the application of a direct actuation of the Braille dot 20 without the need of a pneumatic force. Shape Memory Alloys (SMA's) are a unique class of alloys which have the ability to form two different crystalline phases, defined as martensite and austenite, in response to temperature and strain. SMA's are produced by equiatomically combining at least two component metals into a desired shape which is then annealed. When produced, the SMA is in the austenite phase, having a certain shape and characterized by low ductility, high Young's modulus and high yield stress. Upon cooling the SMA changes to the martensite phase characterized by high ductility, a low Young's modulus and low yield stress. In the martensite phase, the SMA is easily deformed and can take on a different shape from its austenite or original shape by applying an external strain. The SMA will retain this different shape until it is heated to its austenitic transformation temperature. When the SMA is heated to its austenitic transformation temperature the SMA transitions to its austenite phase and transforms back to its original shape.

In FIG. 9A the thin film SMA element 282 is in its martensite phase with the Braille dot 20 retracted. Since the martensite phase is characterized by high ductility, low Young's modulus and low yield stress, the thin film SMA element 282 is easily deformed by external stresses like biasing means 283, shown as a spring in FIG. 9. When heated to its austenitic transfer temperature, the thin film SMA element 282 transitions from its martensite phase to its