

These slots are illustrated in the drawing, but the sleeve may have more, or less slots and may be unitary with only a single slot. Thus, whenever it is fitted into the well and pushed downwardly against the taper, the slot spacing and the inside diameter of the sleeve will decrease. This will effectively grip a thermopile placed with the sleeve into the well. The holding washer 29 is used to effect this pushing and gripping action by bearing against the top of the sleeve; thus, the inside diameter of the holding washer is slightly greater than the inside diameter of the sleeve so as not to interfere with a lead wire extending from the thermopile through a slot 33 of the sleeve. A ring of bolts 34 extend through holes in the holding washer and into tapped holes 35 in the shoulder 27, and these bolts may be tightened to pull the holding washer tightly against the sleeve and to wedge the sleeve between the tapered wall well and the thermopile.

The structural organization of the thermopile includes a central, axially centered, cylindrical core 40, wherein a tubular test cell 41 is snugly fitted as best shown at FIG. 3. The thermopile consists of alternating retention layers and the thermocouple layers placed upon this core 40 and above an enlargement 42 at the bottom of the core, as now described. Each retention layer includes an inner aluminum ring 43, an outer aluminum ring 44 and an insulation disc 45 between them. The thermocouple layers are discs 46 of insulating material which are wire-wrapped as hereinafter described.

To complete the spacer layer, the inner rings 43 are proportioned to fit against the walls of the core 40, and each ring is split, as at 47, to effect a positive, tight fit upon the core 40. The mica insulator discs 45 have an inside diameter proportioned to fit about the inner rings 43 and an outside diameter proportioned to fit within the outer rings 44. The outer rings 44 are proportioned to fit against the inner wall 32 of the sleeve 30, and each ring 44 is split as at radial slot 48 to permit it to vary in diameter and effect a snug, solid contact of the ring within the sleeve 30. The flow of energy, electrical and thermal, from the core of the thermocouple to the heat sink can be accurately measured only if a continuous and solid contact of the several components is maintained, and in the present invention, this is positively attained because the diametrically adjustable sleeve 30 combines with the array of diametrically adjustable outer rings 44, by virtue of respective slots 33 and 48. For example, if through a machining deviation, one ring 44 has a diameter slightly less than the diameter of an adjacent ring 44, the sleeve 30 would, nevertheless, be fitted over both. When the diameter of the sleeve is then decreased by forcing it into the tapered well, it will first grip the larger ring. Because of slot 48, however, the larger ring 44 will decrease in diameter and to the point where the smaller ring 44 is gripped, and such process would continue until all rings 44 in the thermopile are solidly gripped by the sleeve.

The sleeve 30, the core 40, and the inner and outer rings 43 and 44 are of aluminum. This is an ideal material for heat transfer and also ideal because the same are anodized to form insulated oxide surfaces which will transmit heat but will not short out the small voltages generated by the thermocouples. Thus, the thermocouple wires may lay directly upon these anodized surfaces.

The washer-shaped thermocouple discs 46 are formed of mica or a similar insulating material, depending upon the temperatures at which the calorimetric tests are to be made. Each disc has a thermo-responsive wire 49 wrapped about it, and these discs are placed between the retention layers with the wires against the rings 43 and 44. The discs are smaller in diameter than the outside diameter of the rings 44, while the inner, central holes of the discs are larger in diameter than the core 40. Thus, the thermocouple discs 46 provide a small clearance, and each disc 46 is so proportioned as to lie between the inner and outer rings 43 and 44, at each side of it, with the thermocouple wire 49, wrapped about it, being solidly gripped by the several anodized rings.

Each disc is wrapped with a wire 49, from inside to outside, by a series of loops. For example, each disc may have 30 complete, radially directed wraps or loops about the ring-like body of the disc. At the same time, the wire is prepared to produce a thermocouple action. The wire is preferably a commercial type such as 30 gauge constantan wire which is well known for its thermo-responsive actions when coupled with another metal such as copper or silver. A simple mode of producing the bimetallic wire necessary for a thermocouple action is to copper plate or silver plate one side of the wraps of the constantan wire 49. To do this, the other portions of the wrap are masked, as by covering the same with an acetone-soluble glue. Thereafter, an electroplating operation is permitted to proceed in a conventional manner to deposit a layer of copper upon the exposed reaches of the constantan wire wraps. This operation is permitted to continue until the copper layer 50, shown at FIG. 10, is approximately 0.003-inch thick. The result is a large number of thermocouples in a simple, series-connected arrangement.

A number of thermocouple discs 46 are combined to produce the thermopile T with the wire 49 extending from one disc to the next by means of the short wire portion 49' which has a length approximately equal to the thickness of the large aluminum rings 44. For example, in the unit above described, 40 thermocouple discs may be used in the thermopile, and each disc may have thirty wraps of wire 49. When the wire wraps are electroplated, as hereinabove described, a total of 1,200 individual thermocouples will then be produced. The continuous wire 49 will include connective portions 49' between the adjacent discs and when the thermopile is assembled, with the disc between the spacer components, these wire portions 49' may extend from one disc to the other and will pass through the outer ring slots 48 as indicated at FIGS. 7 and 8. Also, the lead wire 49'' from the bottom of the thermopile may extend upwardly to the top thereof through the passage-way formed by a slot 33 of the sleeve for connection with a lead wire 20, as shown at FIGS. 7 and 8.

An important use of the microcalorimeter is to determine the heat which is released when an asphalt adheres to an aggregate. To make such a test, the tubular test cell 41 is partially filled with asphalt and the aggregate is thereafter dropped into the asphalt. Accordingly, it is necessary to provide a means for dropping the aggregate into the liquid asphalt in the test cell 41 in a manner which will not cause any temperature change in the asphalt except that caused by the reaction. Also, because of the exceeding delicacy of the minute measurements, it is necessary to provide a